

Application of Cryogenic Radiometry to Inter-comparison Measurements Related to TSI

Steven R. Lorentz

**L-1 Standards and Technology, Inc.
Lorentz@L-1.biz**

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Introduction

- ✦ Description of a proposed liquid helium cooled cryogenic radiometer suitable for a direct inter-comparison with a TSI flight instrument.
 - ◆ Operating temperature from 2 K to 9 K.
 - ◆ Optimized for both POWER and IRRADIANCE measurement modes.
 - ◆ This instrument will provide the first direct inter-comparison of TSI flight hardware to a standard optical watt at solar flux levels.

CryoRad-TSI Requirements

- ◆ Similar absolute scale as NIST's L-1 CryoRad or POWR
 - ☞ No reduction in any requirement
- ◆ Measure from 10 nW noise floor to 65 mW (1365 W/m²)
- ◆ Capable of measuring both irradiance and power.
- ◆ An 8-mm diameter limiting aperture
- ◆ Single Vacuum Window!
 - ☞ The window transmittance would be the largest uncertainty! (~100 ppm)
 - ☞ Share a single vacuum with a flight/spare instrument. (Only concern is out-gassing of flight instrument)
 - ☞ Wide range of wavelengths would be possible for the inter-comparison, but not necessary, stick to 532 nm.

CryoRad-TSI Performance

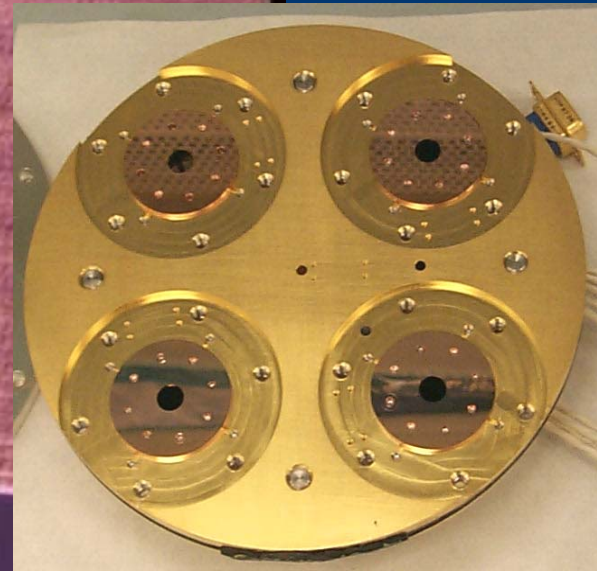
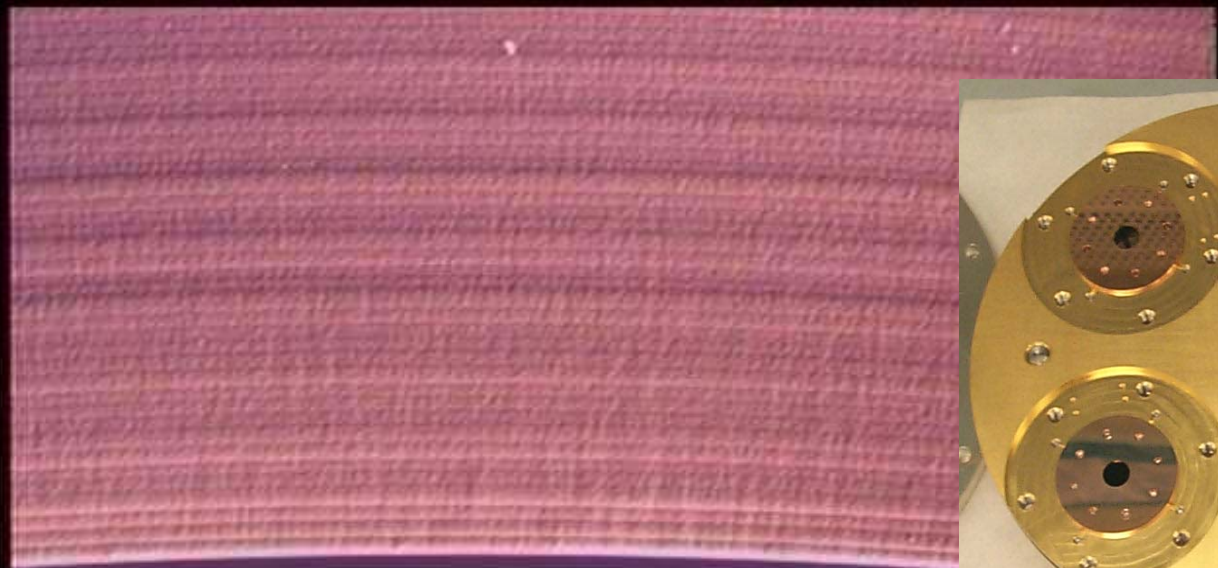
- ◆ Active Heat Sink and Receiver Temp Control
- ◆ New TC-03 electronics will be ready and can be modified for use with this radiometer.
- ◆ Temperature Range 2 K to 9 K
- ◆ 1/e Time Constant < 3 s at 100 mW
- ◆ Cavity Absorptance > 0.999995
- ◆ Noise Floor < 100 nW out of 100 mW
- ◆ Elect./Optical Non-Eq. 0 +/- 5 ppm
- ◆ Elect./Thermal Non-Eq. 0 +/- 5ppm
- ◆ Temperature Sensors GRTs
- ◆ Heaters 1000 Ohms
- ◆ Responsivity 80 K/W

CryoRad-TSI Noise Predictions

◆ Assumptions:

- ☞ Thermal impedance 12.5 mW/K
- ☞ Sensor Resistance 1000 Ohms
- ☞ Sensor Bias 31.6 μA
- ☞ Sensor Power 1 μW
- ☞ Amp Noise 1.9 $\text{nV}/\text{Hz}^{1/2}$
- ☞ Johnson Noise 2.1 $\text{nV}/\text{Hz}^{1/2}$
- ☞ Shot Noise 3.2 $\text{nV}/\text{Hz}^{1/2}$
- ◆ Intrinsic Thermal 66.5 $\text{pW}/\text{Hz}^{1/2}$
- ◆ Total NEP with V-Bias on Sensor 1123 $\text{pW}/\text{Hz}^{1/2}$

Diamond Turned Apertures



8-mm Aperture

Area: 50.0324 mm^2 (2σ) .001%

Material: UBAC Copper Alloy

Optical Microscope at 350X

Step Size is 6 μm

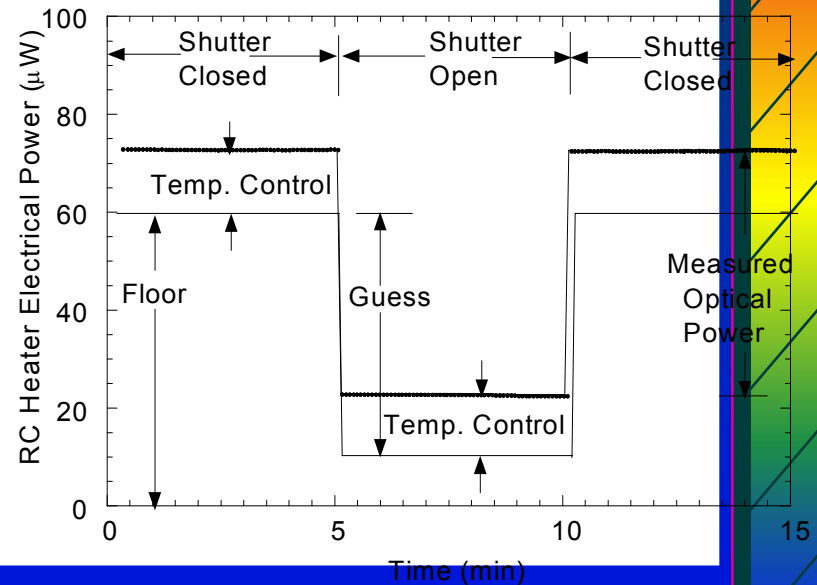
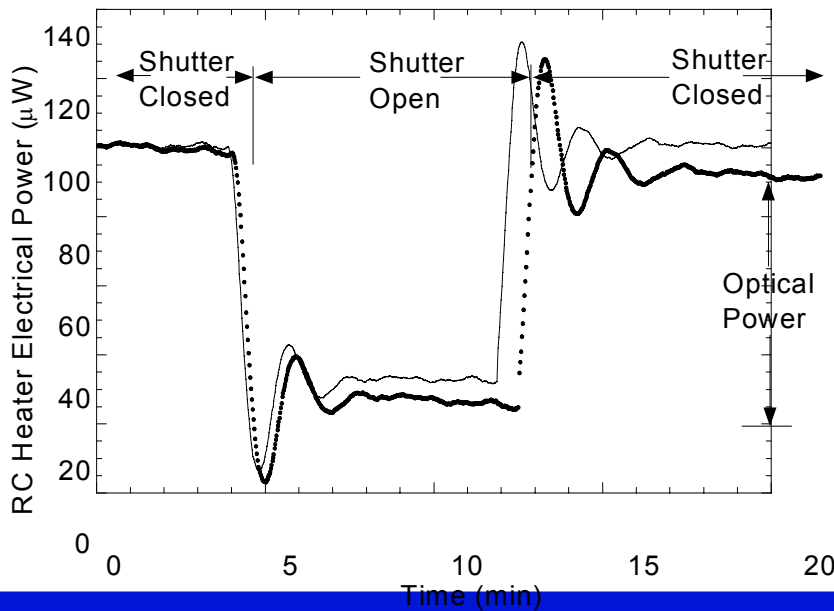
NISTAR
Heat Sink Assembly
with Defining Apertures

Feed-Forward Active Cavity Control Algorithm

(Example data from 300 K prototype built before NISTAR)

Without

With

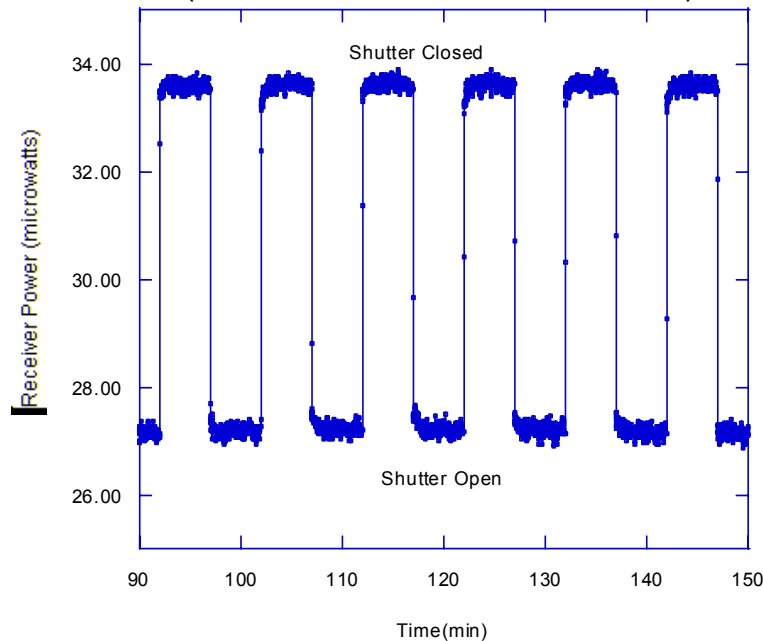


Phase-Sensitive Detection Algorithm used for Demodulation

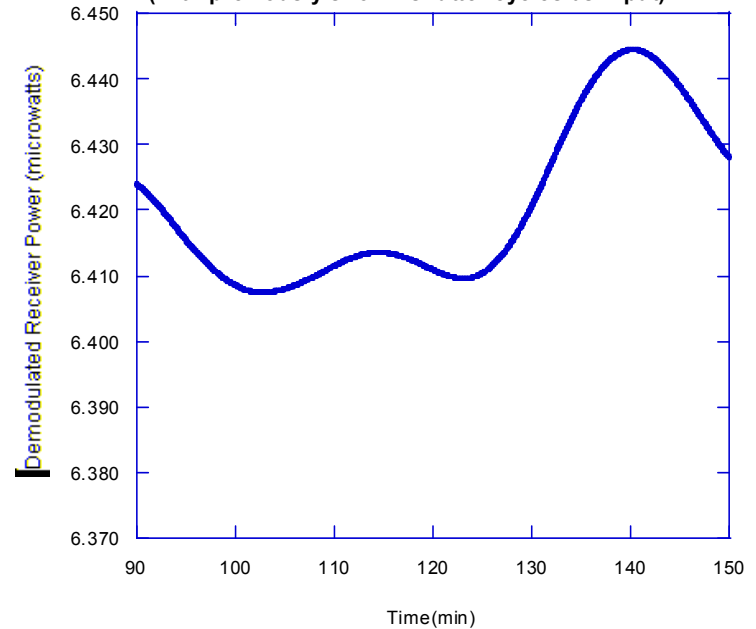
$$r_J = \text{real} \left[\frac{\sum_{M=J-N+1}^J \sum_{L=M}^{M+N-1} \sum_{K=L-N+1}^L \sum_{I=K}^{K+N-1} e^{i2\pi I/N} \phi_I}{\sum_{M=J-N+1}^J \sum_{L=M}^{M+N-1} \sum_{K=L-N+1}^L \sum_{I=K}^{K+N-1} e^{i2\pi I/N} \psi_I} \right]$$

ϕ_I = sequence of measured values
 ψ_I = sequence of shutter position values
 I = raw index
 J = processed index
 N = number of points per shutter cycle
 r_J = demodulated response

Shutter Cycles: Active Cavity with Feed Forward
(Data from NISTAR: HACR 2 will look similar)



Output of 4-boxcar Demodulation Algorithm
(with previously shown shutter cycles as input)

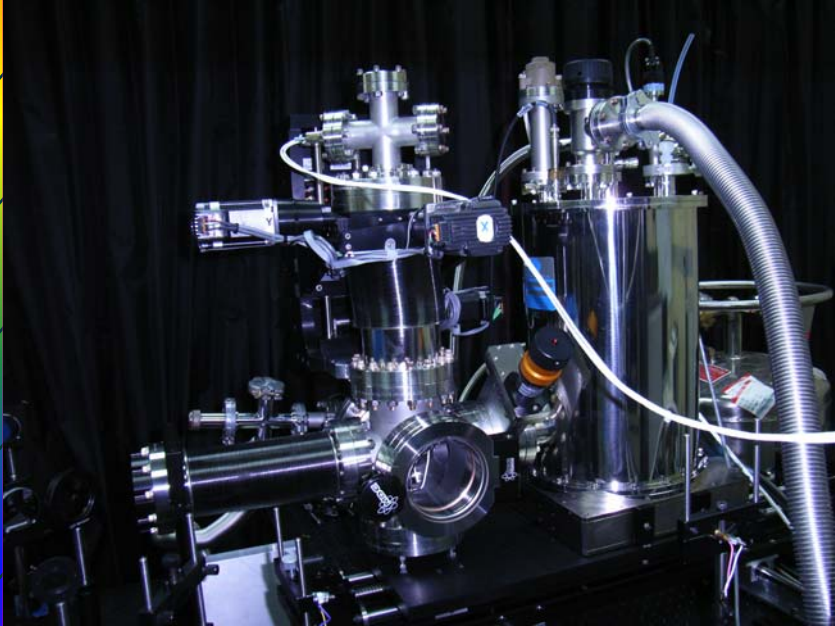


CryoRad-TSI Radiometer Uncertainty Budget for Inter-comparison at 532 nm and 65 mW

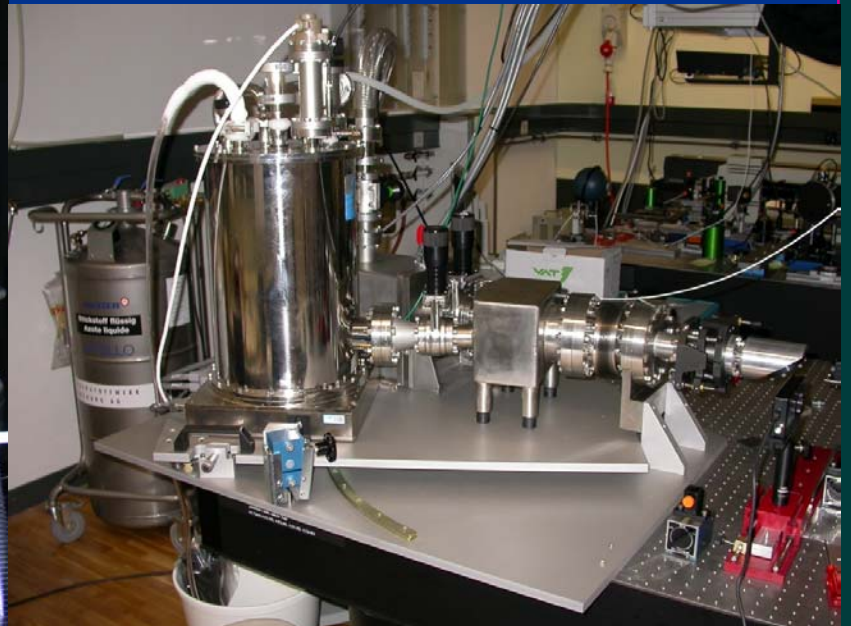
Measurement	Value (Units)	Value (ppm)	Component of Uncertainty (ppm, k=1)	Type
Aperture Area	50 mm ²	1 000 000	30	B
Thermal Contraction (4K)	24 μm (diam.)	6000	50	B/A
Diffraction		<400	40	B
Cavity Reflectance		5	1	A
Electrical Power Linearity	1mW to 65 mW	1 000 000	5	A
Electrical Power Cal	at 65 mW	1 000 000	5	A
Heater Lead Losses		0.0	5	B
E/O Non-Equivalence		0.0	5	A
Scattered Light		100	10	B
Repeatability (Noise)		1 000 000	2	A
		RSS Total	72	

Single Window

- ✦ The use of a common window removes a major uncertainty in modern cryogenic inter-comparisons.



ITRI



METAS

- ✦ CryoRad-TSI – a significant new capability for mission assurance.
- ✦ What Next?
 - ◆ #1) Power mode inter-comparison with silicon trap. (1 month)
 - ◆ #2) Direct inter-comparison at 65 mW. (1 year)
- ✦ Then what?
 - ◆ RETURNABLE cryogenic radiometer!
 - ◆ On-orbit | Aircraft | Balloon
 - ◆ \$\$\$ | \$\$ | \$
 - ◆ 5-10 yrs? | 3 yrs? | 1-2 yrs

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